

# Controlling the transport of an ion: Classical and quantum mechanical solutions

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**Abstract.** We investigate the performance of different control techniques for ion transport in state-of-the-art segmented miniaturized ion traps. We employ numerical optimization of classical trajectories and quantum wavepacket propagation as well as analytical solutions derived from invariant based inverse engineering and geometric optimal control. We find that accurate shuttling can be performed with operation times below the trap oscillation period. The maximum speed is limited by the maximum acceleration that can be exerted on the ion. When using controls obtained from classical dynamics for wavepacket propagation, wavepacket squeezing is the only quantum effect that comes into play for a large range of trapping parameters. We show that this can be corrected by a compensating force derived from invariant based inverse engineering, without a significant increase in the operation time.

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## 1. Introduction

Trapped laser-cooled ions represent a versatile experimental platform offering near-perfect control and tomography of a few body system in the classical and quantum domain [1–4]. The fact that both internal (qubit) and external (normal modes of oscillation) degrees of freedom can be manipulated in the quantum regime allows for many applications in the fields of quantum information processing and quantum simulation [5–7]. Currently, a significant research effort is devoted to scaling these experiments up to larger numbers of qubits. A promising technology to achieve this goal are *microstructured segmented ion traps*, where small ion groups are stored in local potentials and ions are shuttled within the trap by applying suitable voltage ramps to the trap electrodes [8]. In order to enable scalable experiments in the quantum domain, these shuttling operations have to be performed such that the required time is much shorter than the timescales of the relevant decoherence processes. At the same time, one needs to avoid excitation of the ion’s motion after the shuttling operation. These opposing requirements clearly call for the application of advanced control techniques.

Adiabatic ion shuttling operations in a segmented trap have been demonstrated in Ref. [9]. Recent experiments have achieved non adiabatic shuttling of single ions within a few trap oscillation cycles while retaining the quantum ground state of motion [10, 11]. This was made possible by finding ‘sweet spots’ in the shuttling time or removal of the excess energy accumulated during the shuttling by kicks of the trap potential. Given the experimental constraints, it is natural to ask what the speed limitations for the shuttling process are. The impact of quantum effects for fast shuttling operations, i.e., distortions of the wavepacket, also need to be analyzed, and it needs to be assessed whether quantum control techniques [12–14] may be applied to avoid these. Moreover, from a control-theoretical perspective and in view of possible future application in experiment, it is of interest to analyze how optimized voltage ramps can be obtained. Optimal control theory (OCT) combined with classical equations of motion was employed in Ref. [15] to obtain optimized voltage ramps. Quantum effects were predicted not to play a role unless the shuttling takes place on a timescale of a single oscillation period. In Refs. [16, 17], control techniques such as inverse engineering were applied to atomic shuttling problems. The transport of atomic wavepackets in optical dipole potentials was investigated using OCT with quantum mechanical equations of motion [18–20].

The purpose of the present paper is to assess available optimization strategies for the specific problem of transporting a single ion in a microchip ion trap and to utilize them to study the quantum speed limit for this process [21, 22], i.e., to determine the shortest possible time for the transport. Although parameters of the trap architecture of Ref. [23] are used throughout the entire manuscript, we strongly emphasize that the qualitative results we obtain hold over a wide parameter regime. They are thus generally valid for current segmented ion traps, implemented with surface electrode geometry [23, 24] or more traditional multilayer geometry.

The paper is organized as follows. We start by outlining the theoretical framework

in Sec. 2. In particular we review the combination of numerical optimization with classical dynamics in Sec. 2.2 and with wavepacket motion in Sec. 2.3. Analytical solutions to the control problem, obtained from the harmonic approximation of the trapping potential, are presented in Secs. 2.5 and 2.6. Section 3 is devoted to the presentation and discussion of our results. The control solutions for purely classical dynamics of the ion, obtained both numerically and analytically, yield a minimum transport duration as shown in Sec. 3.1. We discuss in Sec. 3.2, how far these solutions correspond to the quantum speed limit. Our results obtained by invariant-based inverse engineering are presented in Sec. 3.3, and we analyze the feasibility of quantum optimal control in Sec. 3.4. Section 4 concludes our paper.

## 2. Methods for trajectory control and wavepacket propagation

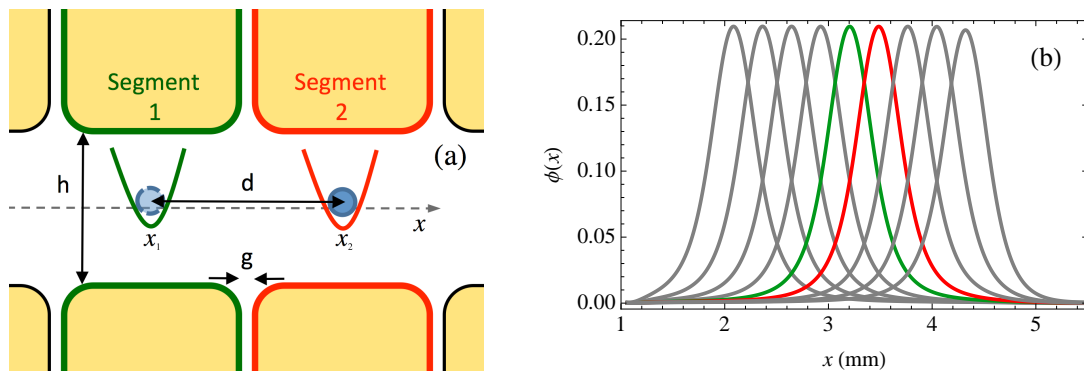
In the following we present the numerical methods we employ to control the transport of a single trapped ion. Besides numerical optimization describing the motion of the ion either with classical mechanics or via wavepacket propagation, we also utilize two analytical methods. This is made possible by the trap geometry which leads to an almost perfectly harmonic trapping potential for the ion at all times.

### 2.1. Prerequisites

We assume ponderomotive confinement of the ion at the rf-node of a linear segmented Paul trap and a purely electrostatic confinement along the trap axis  $x$ , see Fig. 1. This enables us to treat the dynamics only along this dimension. We consider transport of a single ion with mass  $m$  between two neighboring electrodes, which give rise to individual potentials centered at  $x_1$  and  $x_2$ . This may be scaled up to  $N$  electrodes and longer transports without any loss of generality. The ion motion is controlled by a time-dependent electrostatic potential,

$$V(x, t) = U_1(t)\phi_1(x) + U_2(t)\phi_2(x), \quad (1)$$

with segment voltages  $U_i(t)$ , and normal electrode potentials on the trap axis,  $\phi_i(x)$ . They are dimensionless electrostatic potentials obtained with a bias of +1 V at electrode  $i$  and the remaining electrodes grounded (see Fig. 1(b)). These potentials are calculated by using a fast multipole boundary element method [25] for the trap geometry used in recent experiments [10] and shown in Fig. 1. In order to speed up numerics and obtain smooth derivatives, we calculate values for  $\phi_i(x)$  on a mesh and fit rational functions to the resulting data. The spatial derivatives  $\phi'_i(x)$  and  $\phi''_i(x)$  are obtained by differentiation of the fit functions. Previous experiments have shown that the calculated potentials allow for the prediction of ion positions and trap frequencies with an accuracy of one per cent [26, 27] which indicates the precision of the microtrap fabrication process. An increase in the precision can be achieved by calibrating the trapping potentials using resolved sideband spectroscopy. This is sufficient to warrant the application of control techniques as studied here. For the geometry of the trap described in Ref. [10], we



**Figure 1.** (a) Ion shuttling in a segmented linear trap. The dc electrodes form the axial potential for the ion transport along the  $x$ -axis. The rf electrodes for confinement of the ions along the  $x$ -axis are not shown. (b) Axial electrode potentials formed by applying a dc voltage to a facing pair of trap segments. For the specific scenario presented in this manuscript, we use  $d = 280 \mu\text{m}$ ,  $g = 30 \mu\text{m}$  and  $h = 500 \mu\text{m}$ . Each potential is generated from a single pair of segments, depicted in red in (a) and biased to 1 V with all the other dc electrodes grounded.

obtain harmonic trap frequencies of about  $\omega = 2\pi \cdot 1.3 \text{ MHz}$  with a bias voltage of -7 V at a single trapping segment. The individual segments are spaced  $280 \mu\text{m}$  apart. Our goal is to shuttle a single ion along this distance within a time span on the order of the oscillation period by changing the voltages  $U_1$  and  $U_2$ , which are supposed to stay within a predetermined range that is set by experimental constraints. We seek to minimize the amount of motional excitation due to the shuttling process.

## 2.2. Numerical optimization with classical dynamics

Assuming the ion dynamics to be well described classically, we optimize the time dependent voltages in order to reduce the amount of transferred energy. This corresponds to minimizing the functional  $J$ ,

$$J = (E(T) - E_T)^2 + \sum_i \int_0^T \frac{\lambda_a}{S(t)} \Delta U_i(t)^2 dt, \quad (2)$$

i.e., to minimizing the difference between desired energy  $E_T$  and the energy  $E(T)$  obtained at the final time  $T$ .  $\Delta U_i(t) = U_i^{n+1}(t) - U_i^n(t)$  is the update of each voltage ramp in an iteration step  $n$ , and the second term in Eq. (2) limits the overall change in the integrated voltages during one iteration. The weight  $\lambda_a$  is used to tune the convergence and limit the updates. To suppress updates near  $t = 0$  and  $t = T$  the shape function  $S(t) \geq 0$  is chosen to be zero at these points in time. For a predominantly harmonic axial confinement, the final energy is given by

$$E(T) = \frac{1}{2} m \dot{x}^2(T) + \frac{1}{2} m \omega^2 (x(T) - x_2)^2. \quad (3)$$

In order to obtain transport without motional excitation, we choose  $E_T = 0$ . Evaluation of Eq. (3) requires solution of the classical equation of motion. It reads

$$\ddot{x}(t) = -\frac{1}{m} \frac{\partial}{\partial x} V(x, t) \Big|_{x=x(t)} = -\frac{1}{m} \sum_{i=1}^2 U_i(t) \phi'_i(x(t)) \quad (4)$$

for a single ion trapped in the potential of Eq. (1) and is solved numerically using a *Dormand-Prince Runge-Kutta* integrator [25]. Employing Krotov's method for optimal control [28] together with the classical equation of motion, Eq. (4), we obtain the following iterative update rule:

$$\Delta U_i(t) = -\frac{S(t)}{\lambda_a} p_2^{(n)}(t) \phi'_i(x^{(n+1)}(t)), \quad (5)$$

where  $n$  denotes the previous iteration step.  $\mathbf{p} = (p_1, p_2)$  is a costate vector which evolves according to

$$\dot{\mathbf{p}}(t) = - \begin{pmatrix} \frac{p_2}{m} V''(U_i(t), x(t)) \\ p_1 \end{pmatrix}, \quad (6)$$

with its 'initial' condition defined at the final time  $T$ :

$$\mathbf{p}(T) = -2m(E(T) - E_T) \begin{pmatrix} \omega^2(x(T) - x_2) \\ \dot{x}(T) \end{pmatrix}. \quad (7)$$

The algorithm works by propagating  $x(t)$  forward in time, solving Eq. (4) with an initial guess for  $U_i(t)$  and iterating the following steps until the desired value of  $J$  is achieved:

- (i) Obtain  $p(T)$  according to Eq. (7) and propagate  $p(t)$  backwards in time using Eq. (6).
- (ii) Update the voltages according to Eq. (5) at each time step while propagating  $x(t)$  forward in time with the immediately updated voltages.

The optimization algorithm shows rapid convergence and brings the final excitation energy  $E(T)$  as close to zero as desired. An example of an optimized voltage ramp is shown in Fig. 2(a). The voltages obtained are not symmetric under time reversal in contrast to the initial guess. This is rationalized by the voltage updates occurring only during forward propagation which breaks the time reversal symmetry. We find this behavior to be typical for the Krotov algorithm combined with the classical equation of motion.

### 2.3. Numerical optimization of wavepacket propagation

When quantum effects are expected to influence the transport, the ion has to be described by a wave function  $\Psi(x, t)$ . The control target is then to perfectly transfer the initial wavefunction, typically the ground state of the trapping potential centered around position  $x_1$ , to a target wavefunction, i.e., the ground state of the trapping potential centered around position  $x_2$ . This is achieved by minimizing the functional

$$J = 1 - \left| \int_{-\infty}^{\infty} \Psi(x, T)^* \Psi^{\text{tgt}}(x) dx \right|^2 + \int_0^T \frac{\lambda_a}{S(t)} \sum_i \Delta U_i(t)^2 dt. \quad (8)$$

Here,  $\Psi(x, T)$  denotes the wave function of the single ion propagated with the set of voltages  $U_i(t)$ , and  $\Psi^{\text{tgt}}(x)$  is the target wave function. The voltage updates  $\Delta U_i(t)$ , scaling factor  $\lambda_a$  and shape function  $S(t)$  have identical meanings as in Sec. 2.2.  $\Psi(x, T)$  is obtained by solving the time-dependent Schrödinger equation (TDSE),

$$i\hbar \frac{\partial}{\partial t} \Psi(x, t) = \hat{H}(t) \Psi(x, t) = \left( -\frac{\hbar^2}{2m} \frac{d^2}{dx^2} + \sum_{i=1}^N U_i(t) \phi_i(x) \right) \Psi(x, t). \quad (9)$$

As in the classical case, optimization of the transport problem is tackled using Krotov's method [12, 14]. The update equation derived from Eq. (8) is given by

$$\Delta U_i(t) = \frac{S(t)}{\lambda_a} \Im \int_{x_{\min}}^{x_{\max}} \chi^n(x, t)^* \phi_i(x) \Psi^{n+1}(x, t) dx, \quad (10)$$

with  $n$  denoting the iteration step.  $\chi(x, t)$  is a costate wave function obeying the TDSE with 'initial' condition

$$\chi(x, T) = \left[ \int_{x_{\min}}^{x_{\max}} (\Psi(x, T))^* \Psi^{\text{tgt}}(x) dx \right] \Psi^{\text{tgt}}(x, T). \quad (11)$$

Optimized voltages  $U_i(t)$  are obtained similarly to Sec. 2.2, i.e., one starts with the ground state, propagates  $\Psi(x, t)$  forward in time according to Eq. (9), using an initial guess for the voltage ramps, and iterates the following steps until the desired value of  $J$  is achieved:

- (i) Compute the costate wave function at the final time  $T$  according to Eq. (11) and propagate  $\chi(x, t)$  backwards in time, storing  $\chi(x, t)$  at each timestep.
- (ii) Update the control voltages according to Eq. (10) using the stored  $\chi(x, t)$ , while propagating  $\Psi(x, t)$  forward using the immediately updated control voltages.

Equations (10) and (11) imply a sufficiently large initial overlap between the wave function, which is forward propagated under the initial guess, and the target state in order to obtain a reasonable voltage update. This emphasizes the need for good initial guess ramps and illustrates the difficulty of the control problem when large phase space volumes need to be covered.

To solve the TDSE numerically, we use the Chebshev propagator [29] in conjunction with a Fourier grid [30, 31] for efficient and accurate application of the kinetic energy part of the Hamiltonian. Denoting the transport time by  $T$  and the inter-electrode spacing by  $d$ , the average momentum during the shuttling is given by  $\bar{p} = md/T$ . Typical values of these parameters yield a phase space volume of  $d \cdot \bar{p} / \hbar \approx 10^7$ . This requires the numerical integration to be extremely stable. In order to ease the numerical treatment, we can exploit the fact that the wavefunction's spatial extent is much smaller than  $d$  and most excess energy occurs in the form of classical oscillations. This allows for propagating the wave function on a small *moving grid* that extends around the instantaneous position and momentum expectation values [25]. The details of our implementation combining the Fourier representation and a moving grid are described in Appendix A.

#### 2.4. Initial guess voltages

Any optimization, no matter whether it employs classical or quantum equations of motion, starts from an initial guess. For many optimization problems, and in particular when using gradient-based methods for optimization, a physically motivated initial guess is crucial for success of the optimization [32]. Here, we design the initial guess for the voltage ramps such that the ion is dragged from position  $x_1$  to  $x_2$  in a smooth fashion. This is achieved as follows: The trapping potential  $V(x, t)$  can be described by the position of its local minimum  $\alpha(t)$ . Obviously,  $\alpha(t)$  needs to fulfill the boundary conditions  $\alpha(0) = x_1$ ,  $\alpha(T) = x_2$ . In order to ensure smooth acceleration and deceleration of the center of the trap, we also demand  $\dot{\alpha}(0) = \dot{\alpha}(T) = \ddot{\alpha}(0) = \ddot{\alpha}(T) = 0$ . A possible ansatz fulfilling these boundary conditions is given by a polynomial of order 6,

$$\alpha(t) = x_1 + d(10s^3 - 15s^4 + 6s^6), \quad (12)$$

where  $d = x_2 - x_1$  denotes the transport distance and  $s = t/T$  is a dimensionless time.

To derive initial guess voltages  $U_i^0(t)$ , we use as a first condition that the local minimum of the potential coincides with  $\alpha(t)$ . Second, we fix the trap frequency  $\omega$  to a constant value throughout the whole shuttling process,

$$\begin{aligned} \left. \frac{\partial V}{\partial x} \right|_{x=\alpha(t)} &= \phi'_1(\alpha(t))U_1^0(t) + \phi'_2(\alpha(t))U_2^0(t) \stackrel{!}{=} 0, \\ \left. \frac{\partial^2 V}{\partial x^2} \right|_{x=\alpha(t)} &= \phi''_1(\alpha(t))U_1^0(t) + \phi''_2(\alpha(t))U_2^0(t) \stackrel{!}{=} m\omega^2. \end{aligned} \quad (13)$$

These equations depend on first and second order spatial derivatives of the electrode potentials. Solving for  $U_1^0(t)$ ,  $U_2^0(t)$ , we obtain

$$U_i^0(t) = \frac{(-1)^i m\omega^2 \phi'_j(\alpha(t))}{\phi''_2(\alpha(t))\phi'_1(\alpha(t)) - \phi''_1(\alpha(t))\phi'_2(\alpha(t))}, \quad i, j \in \{1, 2\}, \quad j \neq i. \quad (14)$$

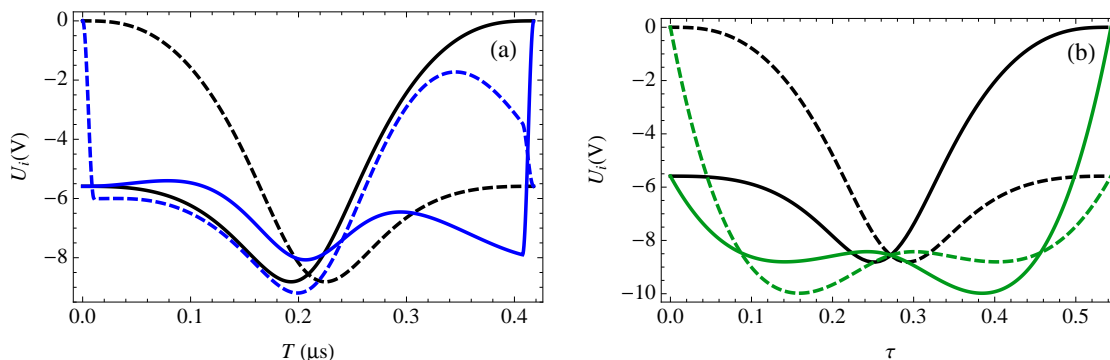
An example is shown in Fig. 2. If the electrode potentials have translational symmetry, i.e.,  $\phi_j(x) = \phi_i(x + d)$ , then  $U_1^0(t) = U_2^0(T - t)$ . This condition is approximately met for sufficiently homogeneous trap architectures.

#### 2.5. Geometric optimal control

Most current ion traps are fairly well described by a simple harmonic model,

$$V(x, t) = -u_1(t)\frac{1}{2}m\omega_0^2(x - x_1)^2 - u_2(t)\frac{1}{2}m\omega_0^2(x - x_2)^2, \quad (15)$$

where  $\omega_0$  is the trap frequency and  $u_i$  are dimensionless control parameters which correspond to the electrode voltages. Since the equations of motion can be solved analytically, one can also hope to solve the control problem analytically. One option is given by Pontryagin's maximum principle [16, 33] which allows to determine time-optimal controls. Compared to numerical optimization which always yields local optima, Pontryagin's maximum principle guarantees the optimum to be global.



**Figure 2.** Control voltages applied to electrodes for transporting a  $^{40}\text{Ca}^+$  ion from electrode 1 (solid lines) to electrode 2 (dashed lines) within 418 ns for an initial trap frequency of  $\omega = 2\pi \cdot 1.3 \text{ MHz}$ : Initial guess voltage ramps (a and b, black) and ramps obtained by classical optimization (a, blue) and the invariant-based inverse engineering (b, green).

In general, the cost functional,

$$J[\mathbf{u}] = \int_0^T g(\mathbf{y}, \mathbf{u}) dt, \quad (16)$$

is minimized for the equation of motion  $\dot{\mathbf{y}} = \mathbf{f}(\mathbf{y}, \mathbf{u})$  and a running cost  $g(\mathbf{y}, \mathbf{u})$  with  $\mathbf{u} = (u_1, u_2)$  and  $\mathbf{y} = (x, v)$  in our case. The optimization problem is formally equivalent to finding a classical trajectory by the principle of least action. The corresponding classical control Hamiltonian that completely captures the optimization problem is given by

$$H_c(\mathbf{p}, \mathbf{y}, \mathbf{u}) = p_0 g(\mathbf{y}, \mathbf{u}) + \mathbf{p} \cdot \mathbf{f}(\mathbf{y}, \mathbf{u}) \quad (17)$$

with costate  $\mathbf{p}$ , obeying

$$\dot{\mathbf{p}} = -\frac{\partial H_c}{\partial \mathbf{y}}, \quad (18)$$

and  $p_0 < 0$  a constant to compensate dimension. Pontryagin's principle states that  $H_c$  becomes maximal for the optimal choice of  $\mathbf{u}(t)$  [16, 33].

Here we seek to minimize the transport time  $T$ . The cost functional then becomes

$$J[\mathbf{u}] = \int_0^{T_{\min}} dt = T_{\min},$$

which is independent of  $\mathbf{u}$  itself and leads to  $g(\mathbf{y}, \mathbf{u}) = 1$ . Inserting the classical equations of motion  $\dot{\mathbf{y}} = (v, -\partial_x V)$ , the control Hamiltonian becomes

$$H_c(\mathbf{p}, \mathbf{y}, \mathbf{u}) = p_0 + p_1 v + p_2 (u_1 \cdot (x - x_1) + u_2 \cdot (x - x_2)) \omega_0^2. \quad (19)$$

We bound  $u_1$  and  $u_2$  by  $u_{\max}$  which corresponds to the experimental voltage limit. Since  $H_c$  is linear in  $u_i$  and  $x_1 \leq x \leq x_2$ ,  $H_c$  becomes maximal depending on the sign of  $p_2$ ,

$$u_1(t) = -u_2(t) = \text{sign}(p_2) u_{\max}. \quad (20)$$



Evaluating Eq. (18) for  $H_c$  of Eq. (19) leads to

$$\dot{p}_1 = p_2 \omega_0^2 (u_1 - u_2) \quad (21)$$

$$\dot{p}_2 = -p_1. \quad (22)$$

In view of Eq. (20), the only useful choice is  $p_2(0) > 0$ . Otherwise the second electrode would be biased to a positive voltage, leading to a repulsive instead of an attractive potential acting on the ion. The equations of motion for the costate thus become

$$\dot{p}_1 = 0 \quad \Rightarrow \quad p_1(t) = c_1 \quad (23)$$

$$\dot{p}_2 = -p_1 \Rightarrow p_2(t) = p_2(0) - c_1 t. \quad (24)$$

For a negative constant  $c_1$ ,  $p_2$  is never going to cross zero. This implies that there will not be a switch in voltages leading to continuous acceleration. For positive  $c_1$  there will be a zero crossing at time  $t_{\text{sw}} = p_2(0)/c_1$ . The optimal solution thus corresponds to a single switch of the voltages. We will analyze this solution and compare it to the solutions obtained by numerical optimization below in Section 3.

### 2.6. Invariant based inverse engineering

For quantum mechanical equations of motion, geometric optimal control is limited to very simple dynamics such as that of three- or four-level systems, see e.g. Ref. [34]. A second analytical approach that is perfectly adapted to the quantum harmonic oscillator utilizes the Lewis-Riesenfeld theory which introduces dynamical invariants and their eigenstates [35]. This invariant-based inverse engineering approach (IEA) has recently been applied to the transport problem [36, 37]. The basic idea is to compensate the inertial force occurring during the transport sequence. To this end, the potential is written in the following form:

$$V(x, t) = -F(t)x + \frac{m}{2}\Omega^2(t)x^2 + \frac{1}{\rho^2(t)}U\left(\frac{x - \alpha(t)}{\rho(t)}\right). \quad (25)$$

The functions  $F$ ,  $\Omega$ ,  $\rho$  and  $\alpha$  have to fulfill constraints,

$$\ddot{\rho}(t) + \Omega^2(t)\rho(t) = \frac{\Omega_0^2}{\rho^3(t)}, \quad (26)$$

$$\ddot{\alpha}(t) + \Omega^2(t)\alpha(t) = F(t)/m, \quad (27)$$

where  $\Omega_0$  is a constant and  $U$  an arbitrary function. We choose  $\Omega(t) = \Omega_0 = 0$ ,  $\rho(t) = 1$ , and  $\alpha(t)$  to be the transport function of Sec. 2.4. This enables us to deduce the construction rule for  $F(t)$ , using Eq. (27),

$$\ddot{\alpha}(t) = F(t)/m, \quad (28)$$

such that  $F(t)$  compensates the inertial force given by the acceleration of the trap center. For the potential of Eq. (25), the Hermitian operator

$$\hat{I} = \frac{1}{2m} [\rho(p - m\dot{\alpha}) - m\dot{\rho}(x - \alpha)]^2 + \frac{1}{2}m\Omega_0^2 \left(\frac{x - \alpha}{\rho}\right)^2 + U\left(\frac{x - \alpha}{\rho}\right) \quad (29)$$

fulfills the invariance condition for all conceivable quantum states  $|\Psi(t)\rangle$ :

$$\frac{d}{dt} \langle \Psi(t) | \hat{I}(t) | \Psi(t) \rangle = 0 \quad \Leftrightarrow \quad \frac{d\hat{I}}{dt} = \frac{\partial \hat{I}}{\partial t} + \frac{1}{i\hbar} [\hat{I}(t), \hat{H}(t)] = 0 \quad (30)$$

with  $\hat{H}$  the Hamiltonian of the ion. The requirement for transporting the initial ground state to the ground state of the trap at the final time corresponds to  $\hat{H}$  and  $\hat{I}$  having a common set of eigenfunctions at initial and final time. This is the case for  $\dot{\alpha}(0) = \dot{\alpha}(T) = \dot{\rho}(t) = 0$  [36, 38]. We can now identify  $U$  in Eq. (25) with the trapping potential of Eq. (1). The additional compensating force is generated using the same trap electrodes by applying an additional voltage  $\delta U_i$ . For a given transport function  $\alpha(t)$  we therefore have to solve the underdetermined equation,

$$m\ddot{\alpha}(t) = -\phi_1'(x(t))\delta U_1(t) - \phi_2'(x(t))\delta U_2(t), \quad (31)$$

where  $x(t)$  is given by the classical trajectory. Since the ion is forced to follow the center of the trap we can set  $x(t) = \alpha(t)$ . The compensating force is supposed to be a function of time only, cf. Eq. (28), whereas changing the electrode voltages by  $\delta U_i$  will, via the  $\phi_i(x)$ , in general yield a position-dependent force. This leads to a modified second derivative of the actual potential:

$$m\omega_c(t)^2 = \sum_{i=1}^2 \phi_i''(\alpha(t))(U_i^0(t) + \delta U_i(t)) = m(\omega^2 + \delta\omega(t)^2), \quad (32)$$

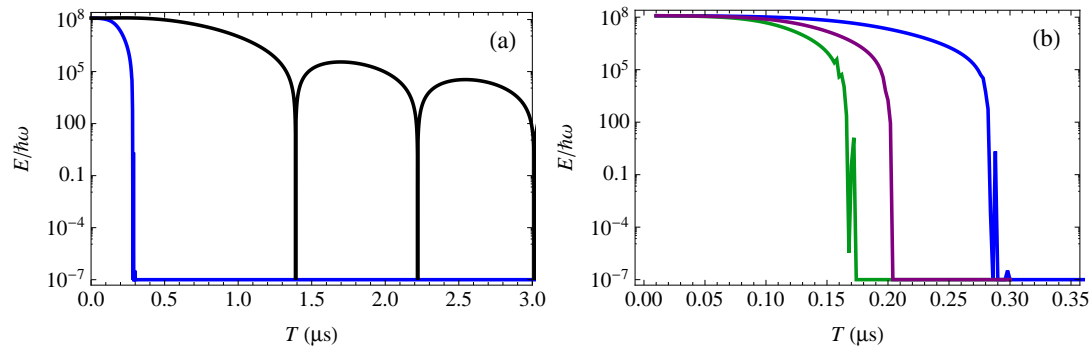
where  $\delta\omega(t)^2$  denotes the change in trap frequency due to the compensation voltages  $\delta U_i$ ,  $\omega$  is the initially desired trap frequency, and  $U_i^0(t)$  is found in Eq. (14). A time-varying actual frequency  $\omega_c(t)$  might lead to wavepacket squeezing. However, since Eq. (31) is underdetermined, we can set  $\delta\omega(t)^2 = 0$  leading to  $\omega_c(t) = \omega$  as desired. With this condition we can solve Eq. (31) and obtain

$$\delta U_i(t) = \frac{\ddot{\alpha}(t) (-1)^i m \phi_j''(\alpha(t))}{\phi_2''(\alpha(t))\phi_1'(\alpha(t)) - \phi_2'(\alpha(t))\phi_1''(\alpha(t))}, \quad i, j \in \{1, 2\}, \quad j \neq i. \quad (33)$$

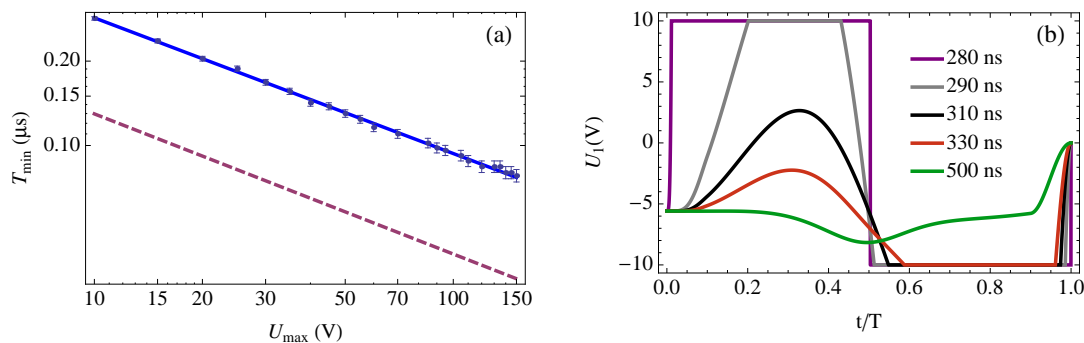
Note that Eq. (33) depends only on the trap geometry. The transport duration  $T$  enters merely as a scaling parameter via  $\ddot{\alpha}(t) = \alpha''(s)/T^2$ . An example of a voltage sequence obtained by this method is shown in figure 2(b). The voltage curves are symmetric under time inversion like the guess voltages, that are derived from the same potential functions  $\phi_i(x)$ .

### 3. Application and comparison of the control methods

We now apply the control strategies introduced in Sec. 2 to a scenario with the parameters chosen to correspond to a typical experimental setting. The scaling of the classical speed limit is studied for a fixed maximum control voltage range and we show how in the limiting case the *bang-bang* solution is obtained. To verify the validity of the classical solution we are applying the obtained voltage ramps to a quantum mechanical wave packet propagation. Similarly, we use the invariant-based approach and verify the result for a quantum mechanical propagation.



**Figure 3.** Final energy vs. transport time for different voltage ramps and classical dynamics. (a) shows the improvement over the initial guess (black) by numerical optimization for a maximum voltage of 10 V (blue) and (b) compares the results of numerical optimization for maximum voltages of 10 V (blue), 20 V (purple), and 30 V (green). The spikes in (b) are due to voltage truncation.



**Figure 4.** (a) Minimum transport time  $T_{\min}^{\text{opt}}$  vs. maximum electrode voltage  $U_{\max}$ , obtained from numerical optimization of classical transport dynamics (blue dots) along with a fit to Eq. (34). We also indicate the analytic bang-bang result, Eq. (37), derived for idealized, purely harmonic potentials (purple dashed line) being proportional to  $1/\sqrt{U_{\max}}$ . The slopes of the curves are clearly similar, indicating the negligible impact of anharmonicities on the scaling of  $T_{\min}^{\text{opt}}$  with  $U_{\max}$ . (b) Optimized voltages for the left electrode with  $U_{\max} = 10$  V: The shorter the transport time, the more the ramp approaches a square shape. The rectangular bang-bang-like solution is attained at  $T = 280$  ns, where the classical control of energy neutral transport breaks down due to an insufficient voltage range.

### 3.1. Experimental constraints and limits to control for classical ion transport

In any experiment, there is an upper limit to the electrode voltages that can be applied. It is the range of electrode voltages that limits the maximum transport speed. Typically this range is given by  $\pm 10$  V for technical reasons. It could be increased by the development of better voltage supplies. We define the minimum possible transport time  $T_{\min}$  to be the smallest time  $T$  for which less than 0.01 phonons are excited due to the total transport. To examine how  $T_{\min}$  scales as a function of the maximum electrode voltages  $U_{\max}$ , we have carried out numerical optimization combined with

classical equations of motion. The initial guess voltages, cf. Eqs. (12) and (14), were taken to preserve a constant trap frequency of  $\omega = 2\pi \cdot 1.3$  MHz for a  $^{40}\text{Ca}^+$  ion. The transport ramps were optimized for a range of maximum voltages between 10-150 V and transport times between 10 ns and 300 ns with voltages truncated to  $\pm U_{\max}$  during the updates. The results are shown in Figs. 3 and 4. Figure 3 depicts the final excitation energy versus transport time, comparing the initial guess (black) to an optimized ramp with  $U_{\max} = 10$  V (blue) in Fig. 3(a). For the initial guess, the final energy displays an oscillatory behavior with respect to the trap period ( $T_{\text{per}} = 0.769 \mu\text{s}$  for  $\omega = 2\pi \cdot 1.3$  MHz) as it has been experimentally observed in Ref. [10], and an overall decrease of the final energy for longer transport times. The optimized transport with  $U_{\max} = 10$  V (blue line in Fig. 3(a)) shows a clear speed up of energy neutral transport: An excitation energy of less than 0.01 phonons is obtained for  $T_{\min}^{\text{opt}} = 0.284 \mu\text{s}$  compared to  $T_{\min}^{\text{guess}} = 1.391 \mu\text{s}$ . The speedup increases with maximum voltage as shown in Fig. 3(b). The variation of  $T_{\min}^{\text{opt}}$  on  $U_{\max}$  is studied in Fig. 4(a). We find a functional dependence of

$$T_{\min}^{\text{opt}}(U_{\max}) \approx a \left( \frac{U_{\max}}{1 \text{ V}} \right)^{-b} \quad (34)$$

with  $a = 0.880(15) \mu\text{s}$  and  $b = 0.487(5)$ . Optimized voltages are shown in Fig. 4(b) for the left electrode with  $U_{\max} = 10$  V. As the transport time decreases, the voltage ramp approaches a square shape. A bang-bang-like solution is attained at  $T = 280$  ns. However, for such a short transport time, classical control of energy neutral transport breaks down due to an insufficient voltage range and the final excitation amounts to 5703 mean phonons.

In the following we show that for purely harmonic potentials, the exponent  $b$  in Eq. (34) is universal, i.e., it does not depend on trap frequency nor ion mass. It is solely determined by the bang-bang like optimized voltage sequences, where instantaneous switching between maximum acceleration and deceleration guarantees shuttling within minimum time. The technical feasibility of bang-bang shuttling is thoroughly analyzed in Ref. [39]. The solution is obtained by the application of Pontryagin's maximum principle [16, 33] as discussed in Sec. 2.5 and assumes instantaneous switches. Employing Eqs. (20) and (24), the equation of motion becomes

$$\ddot{x} = \omega_0^2 u_{\max} \cdot \begin{cases} d, & t < t_{\text{sw}} \\ -d, & t > t_{\text{sw}} \end{cases}. \quad (35)$$

This can be integrated to

$$x(t) = \begin{cases} x_1 + u_{\max} d \omega_0^2 t^2, & 0 \leq t \leq t_{\text{sw}} \\ x_1 + d - u_{\max} d \omega_0^2 (t - T_{\min})^2, & t_{\text{sw}} \leq t \leq T_{\min} \end{cases} \quad (36)$$

with the boundary conditions  $x(0) = x_1$ ,  $x(T_{\min}) = x_2$  and  $\dot{x}(0) = \dot{x}(T_{\min}) = 0$ . Using the continuity of  $\dot{x}$  and  $x$  at  $t = t_{\text{sw}}$ , we obtain

$$t_{\text{sw}} = \frac{T}{2}, \quad T_{\min} = \frac{\sqrt{2}}{\omega_0} \sqrt{\frac{1}{u_{\max}}}. \quad (37)$$

Notably, the minimum transport time is proportional to  $u_{\max}^{-1/2}$  which explains the behavior of the numerical data shown in Fig. 4. This scaling law can be understood intuitively by considering that in the bang-bang control approach, the minimum shuttling time is given by the shortest attainable trap period, which scales as  $u_{\max}^{-1/2}$ . Assuming a trap frequency of  $\omega_0 = 2\pi \cdot 0.55$  MHz in Eq. (37), corresponding to a trapping voltage of  $-1$  V for our trap geometry, we find a prefactor  $\sqrt{2}/\omega_0 = 0.41\mu\text{s}$ . This is smaller than  $a = 0.880(15)\mu\text{s}$  obtained by numerical optimization for realistic trap potentials. The difference can be rationalized in terms of the average acceleration provided by the potentials. For realistic trap geometries, the force exerted by the electrodes is inhomogeneous along the transport path. Mutual shielding of the electrodes reduces the electric field feedthrough of an electrode to the neighboring ones. Thus, the magnitude of the accelerating force that a real electrode can exert on the ion when it is located at a neighboring electrode is reduced with respect to a constant force generating harmonic potential with the same trap frequency.

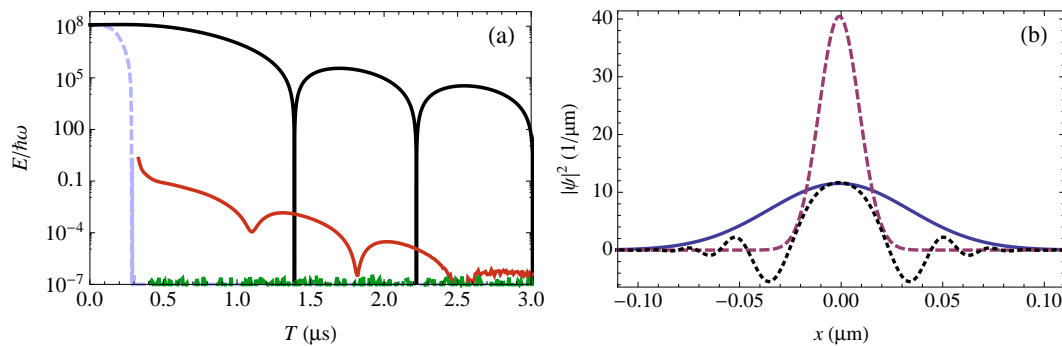
The minimum transport time of  $T_{\min}^{\text{opt}} = 0.284\mu\text{s}$  identified here for  $U_{\max} = 10$  V, cf. the blue line in Fig. 3(a), is significantly shorter than operation times realized experimentally. For comparison, an ion has recently been shuttled within  $3.6\mu\text{s}$ , leading to a final excitation of  $0.10 \pm 0.01$  motional quanta [10]. Optimization may not only improve the transport time but also the stability with respect to uncertainties in the time. This is in contrast to the extremely narrow minima of the final excitation energy for the guess voltage ramps shown in black in Fig. 3(a), implying a very high sensitivity to uncertainties in the transport time. For example, for the fourth minimum of the black curve, located at  $3.795\mu\text{s}$  and close to the operation time of Ref. [10] (not shown in Fig. 3(a)), final excitation energies of less than 0.1 phonons are observed only within a window of 3 ns. Optimization of the voltage ramps for  $T = 3.351\mu\text{s}$  increases the stability against variations in transport time to more than 60 ns.

In conclusion we find that optimizing the classical motion of an ion allows us to identify the minimum operation time for a given maximum voltage and improve the stability with respect to timing uncertainties for longer operation times. The analytical solution derived from Pontryagin's maximum principle is helpful to understand the minimum time control strategy. Numerical optimization accounts for all typical features of realistic voltage ramps. It allows for identifying the minimum transport time, predicting 36.9% of the oscillation period for current maximum voltages and a trap frequency of  $\omega = 2\pi \cdot 1.3$  MHz. This number can be reduced to 12.2% when increasing the maximum voltage by one order of magnitude.

However, these predictions may be rendered invalid by a breakdown of the classical approximation.

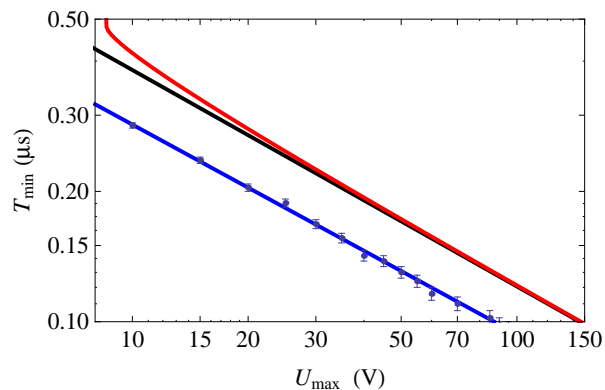
### 3.2. Validity of classical solutions in the quantum regime

We now employ quantum wavepacket dynamics to test the classical solutions, obtained in Sec. 3.1. Provided the trap frequency is constant and the trap is perfectly harmonic,



**Figure 5.** Testing control strategies obtained with classical dynamics for wavepacket motion: (a) Final excitation energy of the ion wavepacket with the initial guess (black) and the optimized voltage ramps with  $U_{\text{max}} = 10$  V (red). Also shown is a solution obtained by invariant based inverse engineering for a quantum mechanical harmonic oscillator (green). For comparison, the final excitation energy obtained by solving the classical equation of motion with the optimized ramp is shown in light blue. Note that for the initial guess (black), the relative difference between wavepacket and classical motion is not visible on the scale of the figure (less than  $10^{-3}$ ). (b) Final wavefunction  $|\Psi(T)|^2$  (blue) for classically optimized transport with  $T = 320$  ns and  $U_{\text{max}} = 10$  V and target wave function  $|\Psi^{\text{tgt}}|^2$  (purple dashed). Also shown is the scaled real part of the final wavefunction  $\Re(\Psi(T))$  (black dotted). The clearly visible spread of the wavepacket corresponds to squeezing of the momentum.

the wave function will only be displaced during the transport. For a time-varying trap frequency, however, squeezing may occur [40]. In extreme cases, anharmonicities of the potential might lead to wavepacket dispersion. Since these two effects are not accounted for by numerical optimization of classical dynamics, we discuss in the following at which timescales such genuine quantum effects become significant. To this end, we have employed the optimized voltages shown in Fig. 4(b) in the propagation of a quantum wavepacket. We compare the results of classical and quantum mechanical motion in Fig. 5(a), cf. the red and lightblue lines. A clear deviation is observed. Also, as can be seen Fig. 5(b), the wavefunction fails to reach the target wavefunction for transport times close to the classical limit  $T_{\text{min}}^{\text{opt}}$ . This is exclusively caused by squeezing and can be verified by inspecting the time evolution of the wavepacket in the final potential: We find the width of the wavepacket to oscillate, indicating a squeezed state. No wavepacket dispersion effects are observed, i.e., the final wavepackets are still minimum uncertainty states, with  $\min(\Delta x \cdot \Delta p) = \hbar/2$ . This means that no effect of anharmonicities in the potential is observed. An impact of anharmonicities is expected once the size of the wavefunction becomes comparable to segment distance  $d$  (see Fig. 1). Then the wavefunction extends over spatial regions in which the potentials deviate substantially from harmonic potentials. For the ion shuttling problem, this effect does not play a role over the relevant parameter regime. The effects of anharmonicities in the quantum regime for trapped ions were thoroughly analyzed in Ref. [41]. Squeezing increases  $T_{\text{min}}$  from  $0.28 \mu\text{s}$  to  $0.86 \mu\text{s}$  for the limit of exciting less than 0.01 phonons, see the red curve in Fig. 5(a), i.e., it only triples the minimum transport time. We show that squeezing



**Figure 6.** Minimum transport time  $T_{\min}$  vs. maximum electrode voltage  $U_{\max}$  obtained by the invariant-based inverse engineering approach: The compensating force method for a trap frequency of  $\omega = 2\pi \cdot 1.3$  MHz using the transport function of Eq. (12) (red) and for the limiting case of vanishing trap frequency (black). Also shown is the classical result from Fig. 4 (blue).

can be suppressed altogether in the following section.

### 3.3. Application of a compensating force approach

In the invariant-based IEA, the minimal transport time is determined by the maximum voltages that are required for attaining zero motional excitation. The total voltage that needs to be applied is given by  $U_i(t) = U_i^0(t) + \delta U_i(t)$  with  $U_i^0(t)$  and  $\delta U_i(t)$  found in Eqs. (14) and (33). The maximum of  $U_i(t)$ , and thus the minimum in  $T$ , is strictly related to the acceleration of the ion provided by the transport function  $\alpha(t)$ , cf. Eq. (33). If the acceleration is too high, the voltages will exceed the feasibility limit  $U_{\max}$ . At this point it can also be understood why the acceleration should be zero at the beginning and end of the transport: For  $\ddot{\alpha}(0) \neq 0$  a non-vanishing correction voltage  $\delta U_i \neq 0$  is obtained from Eq. (33). This implies that the voltages do not match the initial trap conditions, where the ion should be located at the center of the initial potential.

We can derive a transport function  $\alpha(t)$  compliant with the boundary conditions using Eq. (12). For this case, Fig. 6 shows the transport time  $T_{\min}^{\text{IEA}}$  versus the maximum voltage  $U_{\max}$  that is applied to the electrodes during the transport sequence. For large transport times, the initial guess voltages  $U_i^0(t) \propto \omega^2$  dominate the compensation voltages  $\delta U_i(t) \propto \ddot{\alpha}(t) = \alpha''(s)/T^2$ . This leads to the bend of the red curve. When the trap frequency  $\omega$  is lowered, the bend decreases. For the limiting case of no confining potential  $\omega = U_i^0(t) = 0$ ,  $T_{\min}^{\text{IEA}}$  is solely determined by the compensation voltages. In this case the same scaling of  $T_{\min}^{\text{IEA}}$  with  $U_{\max}$  as for the optimization of classical dynamics is observed, cf. black and blue lines in Fig. 6. For large  $U_{\max}$ , this scaling also applies to the case of non-zero trap frequency, cf. red line in Fig. 6.

We have tested the performance of the compensating force by employing it in the time evolution of the wavefunction. It leads to near-perfect overlap with the target state

with an infidelity of less than  $10^{-9}$ . The final excitation energy of the propagated wave function is shown in Fig. 5 (green line) for a maximum voltage of  $U_{\max} = 10$  V. For the corresponding minimum transport time,  $T_{\min}^{\text{IEA}}(10 \text{ V}) = 418$  ns, a final excitation energy six orders of magnitude below that found by optimization of the classical dynamics is obtained. This demonstrates that the invariant-based IEA is capable of avoiding the wavepacket squeezing that was observed in Sec. 3.2 when employing classically optimized controls in quantum dynamics. It also confirms that anharmonicities do not play a role since these would not be accounted for by the IEA-variant employed here. Note that an adaptation of the invariant-based IEA to anharmonic traps is found in Ref. [37]. Similarly to numerical optimization of classical dynamics, IEA is capable of improving the stability against variations in transport time  $T$ . The final excitation energy obtained for  $T = 3.351 \mu\text{s}$  stays below 0.1 phonons within a window of more than 13 ns.

A further reduction of the minimum transport time may be achieved due to the freedom of choice in the transport function  $\alpha(t)$ , by employing higher polynomial orders in order to reduce the compensation voltages  $\delta U_i(t)$ , cf. Eq. (33). However, the fastest quantum mechanically valid transport has to be slower than the solutions obtained for classical ion motion. This follows from the bang-bang control being the time-optimal solution for a given voltage limit and the IEA solutions requiring additional voltage to compensate the wavepacket squeezing. We can thus conclude that the time-optimal quantum solution will be inbetween the blue and black curves of Fig. 6.

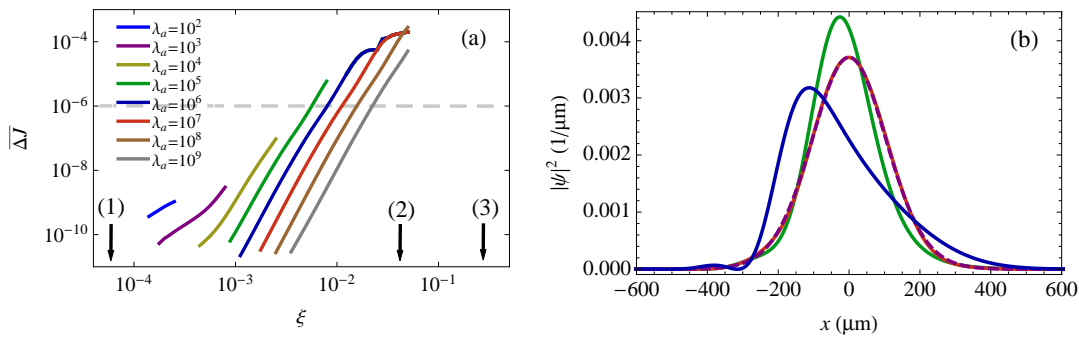
### 3.4. Feasibility analysis of quantum optimal control

Numerical optimization of the wavepacket motion is expected to become necessary once the dynamics explores spatial regions in which the potential is strongly anharmonic or is subject to strongly anharmonic fluctuations. This can be expected, for example, when the spatial extent of the wavefunction is not too different from that of the trap. Correspondingly, we introduce the parameter  $\xi = \sigma_0/d$ , which is the wavefunction size normalized to the transport distance. While for current trap architectures, such a scenario is rather unlikely, further miniaturization might lead to this regime. Also, it is currently encountered in the transport of neutral atoms in tailored optical dipole potentials [42, 43].

Gradient-based quantum OCT requires an initial guess voltage that ensures a finite overlap of the propagated wave function  $\Psi(T)$  with the target state  $\Psi^{\text{tgt}}$ , see Eq. (11). Otherwise, the amplitude of the co-state  $\chi$  vanishes. The overlap can also be analyzed in terms of phase space volume. For a typical ion trap setting with parameters as in Fig. 1, the total covered phase space volume in units of Planck's constant is  $m d^2 \omega / 2\pi h \approx 10^7$ . This leads to very slow convergence of the optimization algorithm, unless an extremely good initial guess is available.

We utilize the results of the optimization for classical dynamics of Sec. 3.1 as initial guess ramps for optimizing the wavepacket dynamics and investigate the convergence rate as a function of the system dimension, i.e., of  $\xi$ . The results are shown in Fig. 7(a),





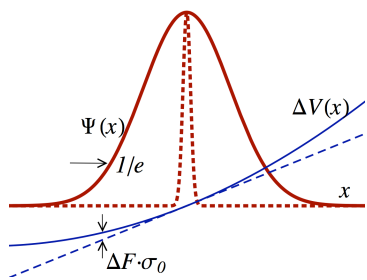
**Figure 7.** (a) Mean improvement of the optimization functional,  $\overline{\Delta J}$  (averaged over 100 iterations), versus relative size of the wavepacket  $\xi$  for different optimization weights  $\lambda_a$ , cf. Eq. (10), ranging from  $\lambda_a = 10^2$  (leftmost line) to  $\lambda_a = 10^9$  (rightmost line) in powers of ten. The arrows indicate: (1) the parameters corresponding to current trap technology, (2) good convergence of quantum OCT with the invariant-based IEA still being valid, (3) fast convergence of quantum OCT with invariant-based IEA starting to fail. (b) Final wavefunction amplitudes for  $\xi = 0.4$  (arrow (3) in (a)) and classical optimization (blue, fidelity of 83.8%), IEA (green, 94.6%), quantum OCT (red, fidelity of 99.9%). Also plotted is the target state (purple dashed).

plotting the mean improvement per optimization step,  $\Delta J$ , averaged over 100 iterations, versus the scale parameter  $\xi$ . We computed the convergence rate  $\overline{\Delta J}$  for different, fixed optimization weights  $\lambda_a$  in Eq. (10). The curves in Fig. 7(a) are truncated for large values of  $\overline{\Delta J}$ , where the algorithm becomes numerically unstable. Values below  $\overline{\Delta J} = 10^{-6}$  (dashed grey line in Fig. 7(a)) indicate an insufficient convergence rate for which no significant gain of fidelity is obtained with reasonable computational resources. In this case the potentials are insufficiently anharmonic to provide *quantum* control of the wavefunction.

Numerical optimization of the wavepacket dynamics is applicable and useful for scale parameters of  $\xi \approx 0.05$  and larger, indicated by arrows (2) and (3) in Fig. 7(a). Then the wavefunction size becomes comparable to the transport distance, leading for example to a phase space volume of around  $10 h$  for arrow (2). At this scale the force becomes inhomogeneous across the wavepacket. This leads to a breakdown of the IEA, as illustrated for  $\xi = 0.4$  in Figs. 7(b) and 8. The fidelity  $\mathfrak{F}_{\text{IEA}}$  for the IEA drops below 94.6%, whereas  $\mathfrak{F}_{\text{qOCT}} = 0.999$  is achieved by numerical optimization of the quantum dynamics.

#### 4. Summary and Conclusions

Manipulation of motional degrees of freedom is very widespread in trapped-ion experiments. However, most theoretical calculations involving ion transport over significant distances are based on approximations that in general do not guarantee the level of precision needed for high-fidelity quantum control, especially in view of applications in the context of quantum technologies. As a consequence, before our work



	$\xi$	$\Delta F/F$	$\mathfrak{F}_{\text{IEA}}$	$\mathfrak{F}_{\text{qOCT}}$	$T_{\text{CPU}}(h)$
(1)	$5.0 \cdot 10^{-5}$	$2.7 \cdot 10^{-13}$	1.000	N/A	N/A
(2)	$5.0 \cdot 10^{-2}$	$2.7 \cdot 10^{-4}$	1.000	0.999	32.2
(3)	$4.0 \cdot 10^{-1}$	$1.2 \cdot 10^{-1}$	0.946	0.999	4.3

**Figure 8.** Limitation of the compensating force approach. A force inhomogeneity  $\Delta F = \sum_i [\phi'_i(\alpha(t) + \sigma_0) - \phi'_i(\alpha(t) - \sigma_0)] \delta U_i(t)$  across the wavefunctions is caused by anharmonicities of the potential  $\Delta V = F(t)x$  used to implement the compensating force. The relative spread of the force  $\Delta F/F$  across the wavefunction is taken at the point in time, where the acceleration  $\ddot{\alpha}(t)$  is maximal.  $\Delta F/F$  increases to the range of several percent for large wavefunction extents. This leads to a drop in the fidelity  $\mathfrak{F}_{\text{IEA}}$ . Also shown is the fidelity  $\mathfrak{F}_{\text{qOCT}}$  obtained by optimizing the quantum dynamics. The CPU time  $T_{\text{CPU}}$  required for optimization could be easily reduced by a factor of 8 in case (3) compared to case (2) due to the better convergence of quantum OCT in this regime.

little was known about how to apply optimal control theory to large-scale manipulation of ion motion in traps, concerning in particular the most efficient simulation and control methods to be employed in different parameter regimes, as well as the level of improvement that optimization could bring.

With this in mind, in the present work we have investigated the applicability of several classical and quantum control techniques for the problem of moving an ion across a trap in a fast and accurate way. When describing the ion dynamics purely classically, numerical optimization yields transport times significantly shorter than a trapping period. The minimum transport duration depends on the maximal electrode voltage that can be applied and was found to scale as  $1/\sqrt{U_{\text{max}}}$ . The same scaling is observed for time-optimal bang-bang-like solutions that can be derived using Pontryagin's maximum principle and assuming perfectly harmonic traps. Not surprisingly, the classically optimized solutions were found to fail when tested in quantum wavepacket motion for transport durations of about one third of a trapping period. Wavepacket squeezing turns out to be the dominant source of error with the final wavepacket remaining a minimum uncertainty state. Anharmonic effects were found to play no significant role for single-ion shuttling over a wide range of parameters. Wavepacket squeezing can be perfectly compensated by the control strategy obtained with the invariant-based inverse engineering approach. It amounts to applying correction voltages which can be generated by the trapping electrodes and which exert a compensating force on the ion. This is found to be the method of choice for current experimental settings.

Control methods do not only allow to assess the minimum time required for ion transport but can also yield more robust solutions. For transport times that have been used in recent experiments [10], significantly larger than the minimum times identified here, the classical solutions are valid also for the quantum dynamics. In this regime, both

numerical optimization of classical ion motion and the inverse engineering approach yield a significant improvement of stability against uncertainties in transport time. Compared to the initial guess voltages, the time window within which less than 0.1 phonons are excited after transport is increased by a factor of twenty for numerical optimization and a factor of five for the inverse engineering approach.

Further miniaturization is expected to yield trapping potentials where the wavepacket samples regions of space in which the potential, or potential fluctuations, are strongly anharmonic. Also, for large motional excitations recent experiments have shown nonlinear Duffing oscillator behavior [44], nonlinear coupling of modes in linear ion crystals [45, 46] and amplitude dependent modifications of normal modes frequencies and amplitude due to nonlinearities [47]. In these cases, numerical optimization of the ion's quantum dynamics presents itself as a well-adapted and efficient approach capable of providing high-fidelity control solutions.

The results presented in this paper provide us with a systematic recipe, based on a single parameter (the relative wave packet size  $\xi$ ), to assess which simulation and control methods are best suited in different regimes. We observe a crossover between applicability of the invariant-based IEA, for a very small wavefunction extension, and that of quantum OCT, when the width of the wave function becomes comparable with the extension of the potential. Both methods combined cover the full range of conceivable trap parameters. That is, no matter what are the trapping parameters, control solutions for fast, high-fidelity transport are available. In particular, in the regime  $\xi \ll 1$ , relevant for ion transport in chip traps, solutions obtained with the inverse engineering approach are fully adequate for the purpose of achieving high-fidelity quantum operations. This provides a major advantage in terms of efficiency over optimization algorithms based on the solution of the Schrödinger equation. The latter in turn becomes indispensable when processes involving motional excitations inside the trap and/or other anharmonic effects are relevant. In this case, the numerical quantum OCT method demonstrated in this paper provides a comprehensive way to deal with the manipulation of the ions' external states.

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**Table A1.** Necessary steps for wavepacket propagation over long distances.

	Mathematical step	Possible implementation
1. Calculate position mean	$\langle x \rangle = \langle \Psi   \hat{x}   \Psi \rangle$	$\langle x \rangle = \sum_i x_i \Psi_i^* \Psi_i$
2. Transform to momentum space		$\{\Phi_i\} = \mathcal{F}\mathcal{F}\mathcal{T}(\{\Psi_i\})$
3. Calculate momentum mean	$\langle p \rangle = \langle \Psi   \hat{p}   \Psi \rangle$	$\langle p \rangle = \sum_i \hbar k_i \Phi_i^* \Phi_i$
4. Shift position	$ \Psi\rangle \rightarrow \exp\left(\frac{i}{\hbar}\langle x \rangle \hat{p}\right)  \Psi\rangle$	$\Phi_i \rightarrow \exp(ik_i \langle x \rangle) \Phi_i$
5. Transform to position space		$\{\Psi_i\} = \mathcal{F}\mathcal{F}\mathcal{T}^{-1}(\{\Phi_i\})$
6. Shift momentum	$ \Psi\rangle \rightarrow \exp\left(\frac{i}{\hbar}\langle p \rangle \hat{x}\right)  \Psi\rangle$	$\Psi_i \rightarrow \exp\left(\frac{i}{\hbar}\langle p \rangle x_i\right) \Psi_i$
7. Update classical quantities		$x_{cl+} = \langle x \rangle, p_{cl+} = \langle p \rangle$

## Appendix A. Quantum wavepacket propagation with a moving Fourier grid

For transport processes using realistic trap parameters, naive application of the standard Fourier grid method [30, 31] will lead to unfeasible grid sizes. This is due to the transport distance being usually 3 to 5 orders of magnitude larger than the spatial width of the wavepacket and possible acceleration of the wavepacket requiring a sufficiently dense coordinate space grid. To limit the number of grid points, a *moving grid* is introduced. Instead of using a spatial grid that covers the entire transport distance, the grid is defined to only contain the initial wavepacket, in a window between  $x_{\min}$  and  $x_{\max}$ . The wavepacket  $\Psi(x, t_0)$  is now propagated for a single time step to  $\Psi(x, t_0 + dt)$ . For the propagated wave function, the expectation value

$$\langle x \rangle = \int_{x_{\min}}^{x_{\max}} \Psi^*(x, t_0 + dt) x \Psi(x, t_0 + dt) dx \quad (\text{A.1})$$

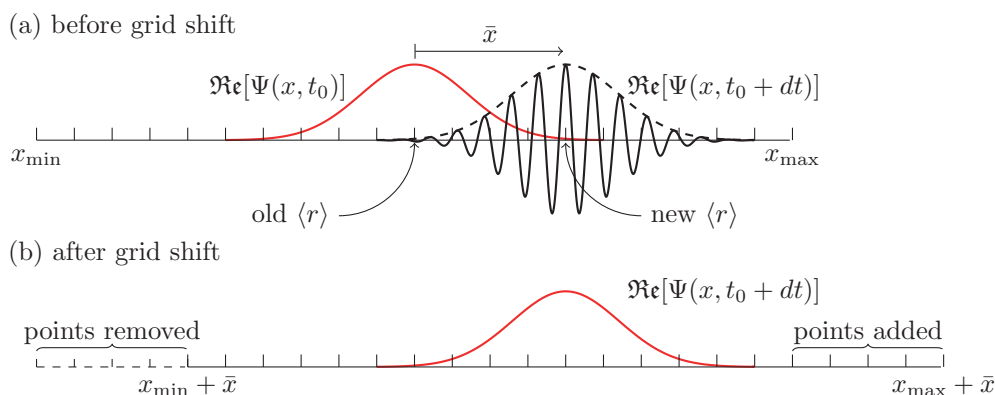
is calculated, and from that an offset is obtained,

$$\bar{x} = \langle x \rangle - \frac{x_{\max} - x_{\min}}{2}, \quad (\text{A.2})$$

by which  $x_{\min}$  and  $x_{\max}$  are shifted. The wavepacket is now moved to the center of the new grid, and the propagation continues to the next time step.

The same idea can also be applied to momentum space. After the propagation step, the expectation value  $\langle k \rangle$  is calculated and stored as an offset  $\bar{k}$ . The wave function is then shifted in momentum space by this offset, which is achieved by multiplying it by  $e^{-i\bar{k}x}$ . This cancels out the fast oscillations in  $\Psi(x, t_0 + dt)$ . When applying the kinetic operator in the next propagation step, the offset has to be taken into account, i.e., the kinetic operator in momentum space becomes  $(k + \bar{k})^2/2m$ .

The combination of the moving grid in coordinate and momentum space allows to choose the grid window with the mere requirement of being larger than the extension of the wavepacket at any point of the propagation. We find typically 100 grid points to be sufficient to represent the acceleration within a single time step. The procedure is illustrated in Fig. A1 and the steps of the algorithm are summarized in Table A1.



**Figure A1.** Illustration of the moving grid procedure. The propagation of the wave function  $\Psi(x, t_0)$  for a single time step is shown in (a). The resulting wave function has moved in position and has non-zero momentum. After shifting the grid in coordinate and momentum space, the propagated wave function is now centered on the new grid and has zero momentum (b).

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